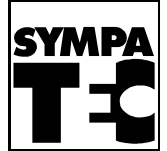


Laser diffraction history and fundamentals,
Fraunhofer physics, Mie-theory



Sympatec

Way
of
Laser Diffraction

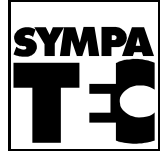
HST: Halley Comet



Sympatec Way of Laser Diffraction

- ★ History of laser diffraction
- ★ Fundamentals
 - ☆ Generation of diffraction patterns
 - ☆ Diffraction pattern
 - ☆ Intensity distributions
 - ☆ Detection
 - ☆ HELOS auto-focus unit
 - ☆ HELOS/RODOS-system
- ★ Comparison of particle size analysis (psa) methods
- ★ Epochs of application
- ★ Fraunhofer Submicron
 - ☆ Mie theory
 - ☆ HELOS-MIE software module
 - ☆ Check list





Laser Diffraction History

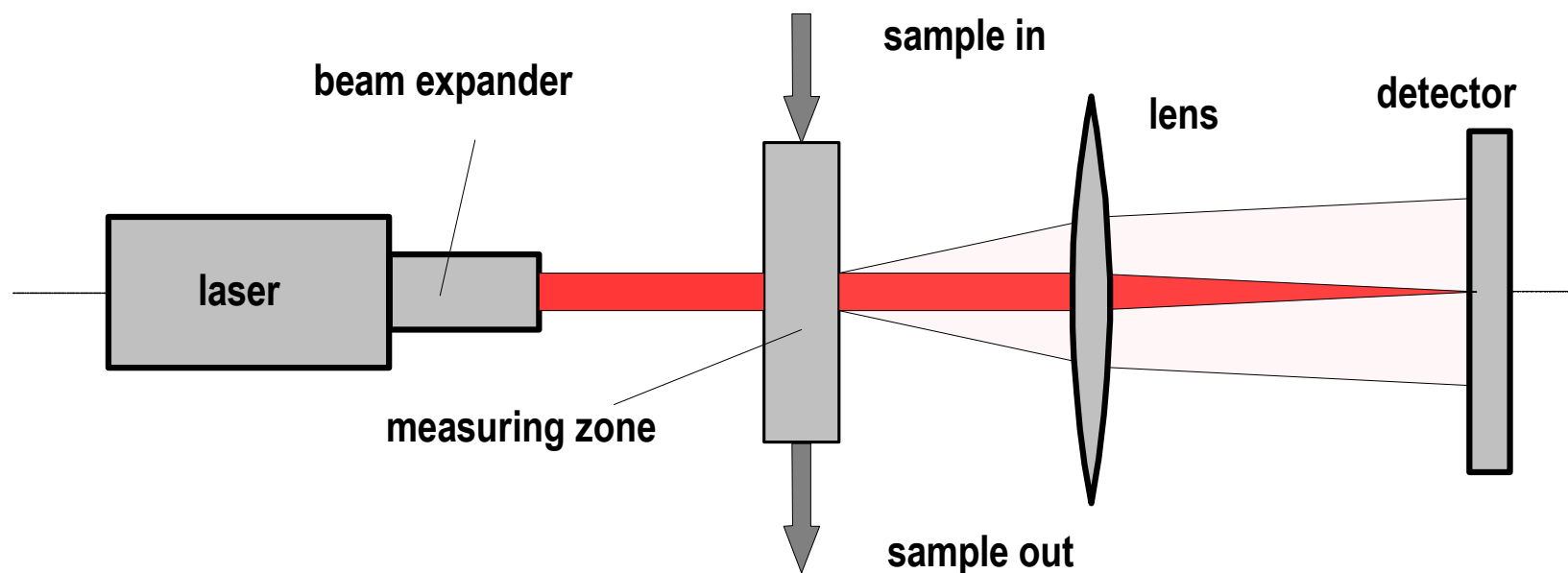
Advanced analysis principle for fast determination of particle size distributions in a wide size range from 0.1 - 10000 μm

| Elements | Definition | Year |
|---------------|---|-------------------|
| Theory | Fraunhofer diffraction physics | 1820 |
| Method | He-Ne-laser as high energy, coherent light for the generation of particle-light interaction | 1960 |
| Sensor | multi-element semiconductor first used as aiming device for military application | 1965 |
| Processing | high performance microcomputers | 1970 |
| Result | particle size analysis with laser diffraction | since 1972 |



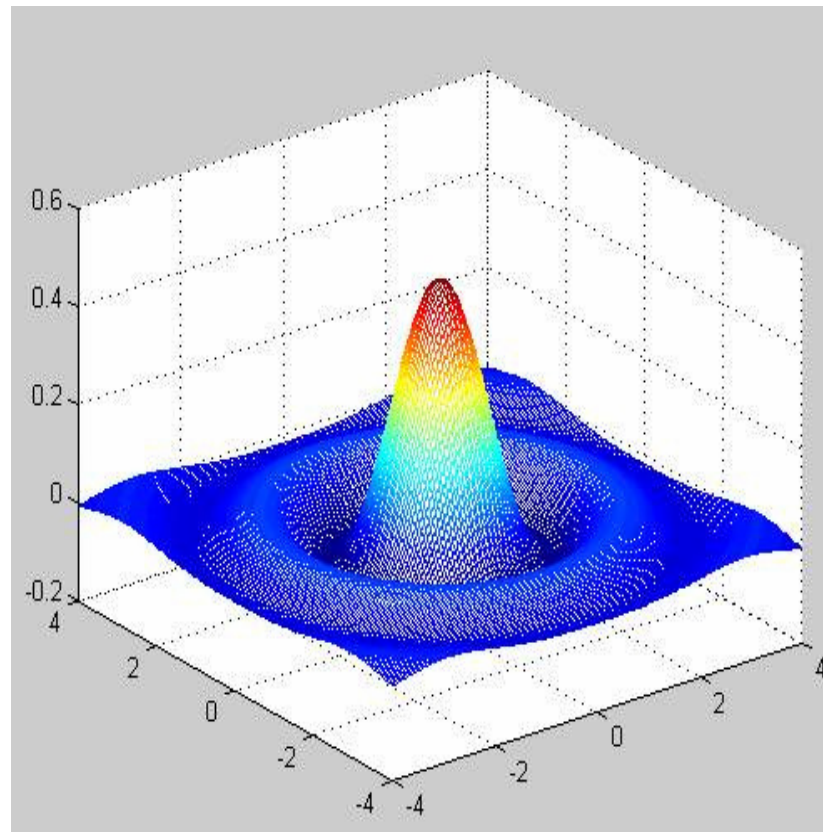
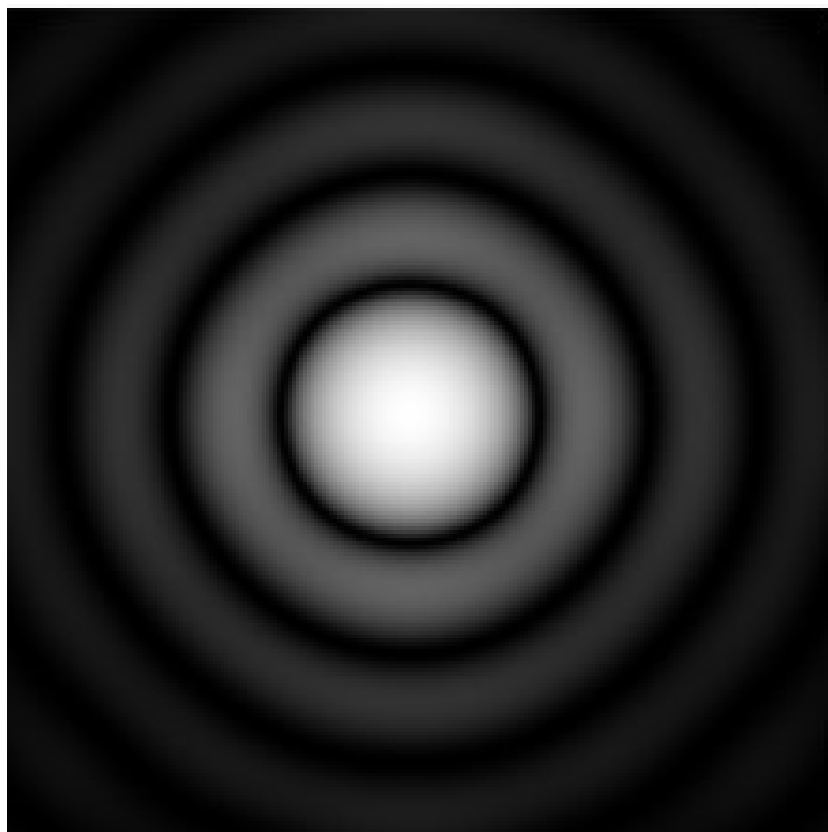
Optical set up for the generation of diffraction patterns

(refer to ISO 13320-1*, § 5, fig. 2)



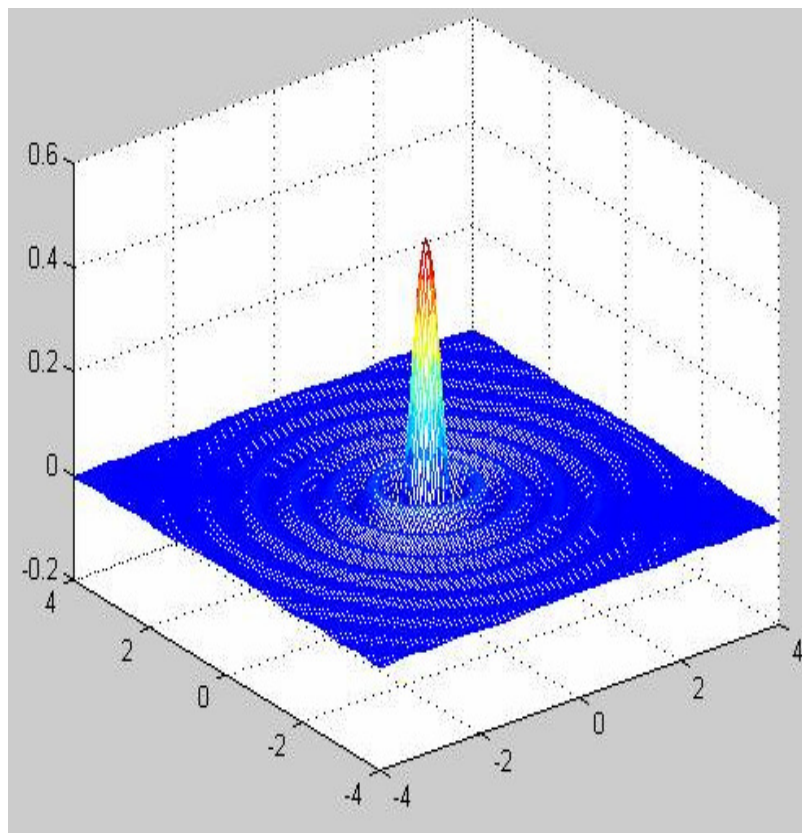
* ISO 13320-1 covers particle sizes from 0.1 μm to approximately 3.0 mm



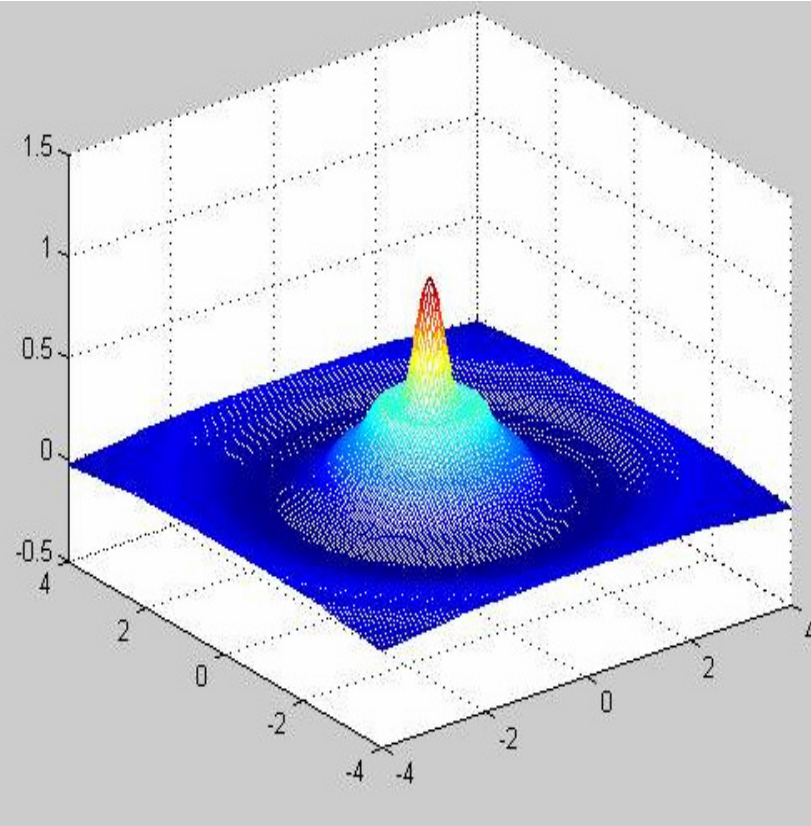


Diffraction Pattern of small spherical Particles



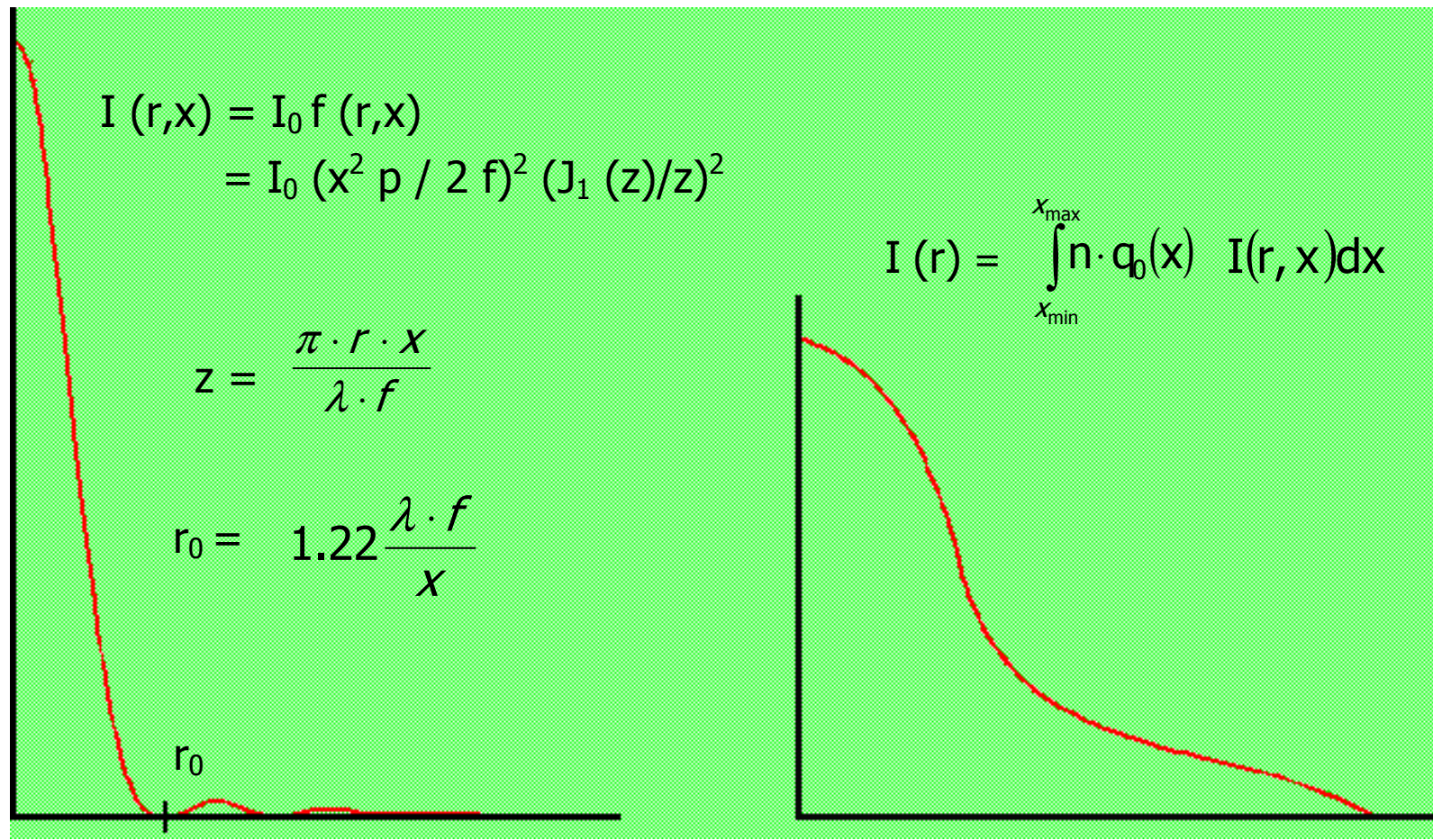


Single coarse particle



Overlay of fine & coarse particle



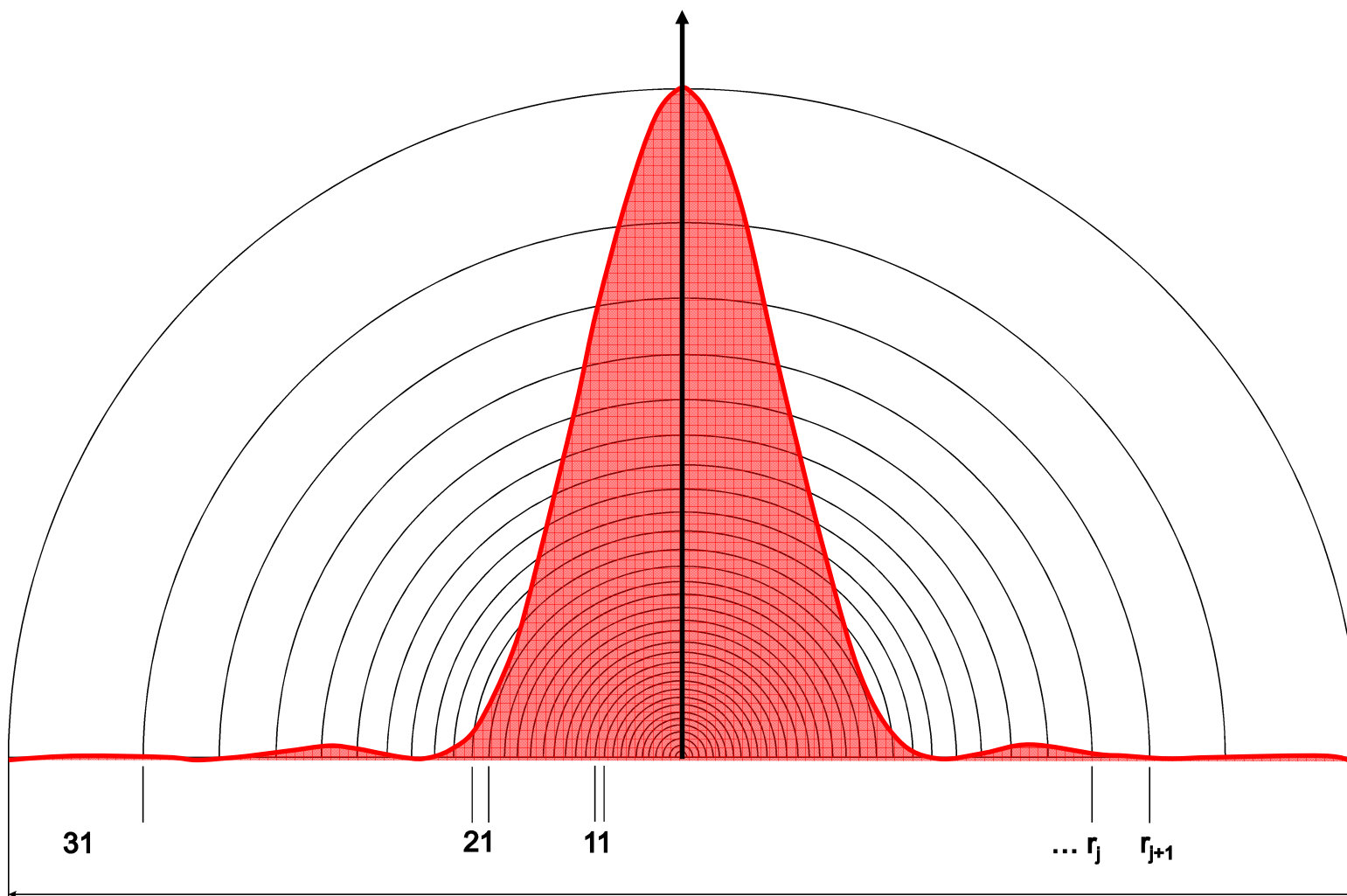


single particle of diameter x

particle size distribution $q_0(x)$

Intensity distribution of Fraunhofer diffraction patterns

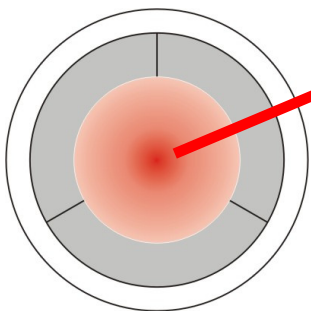
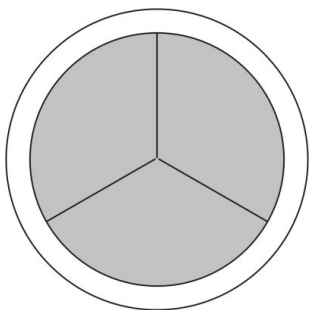




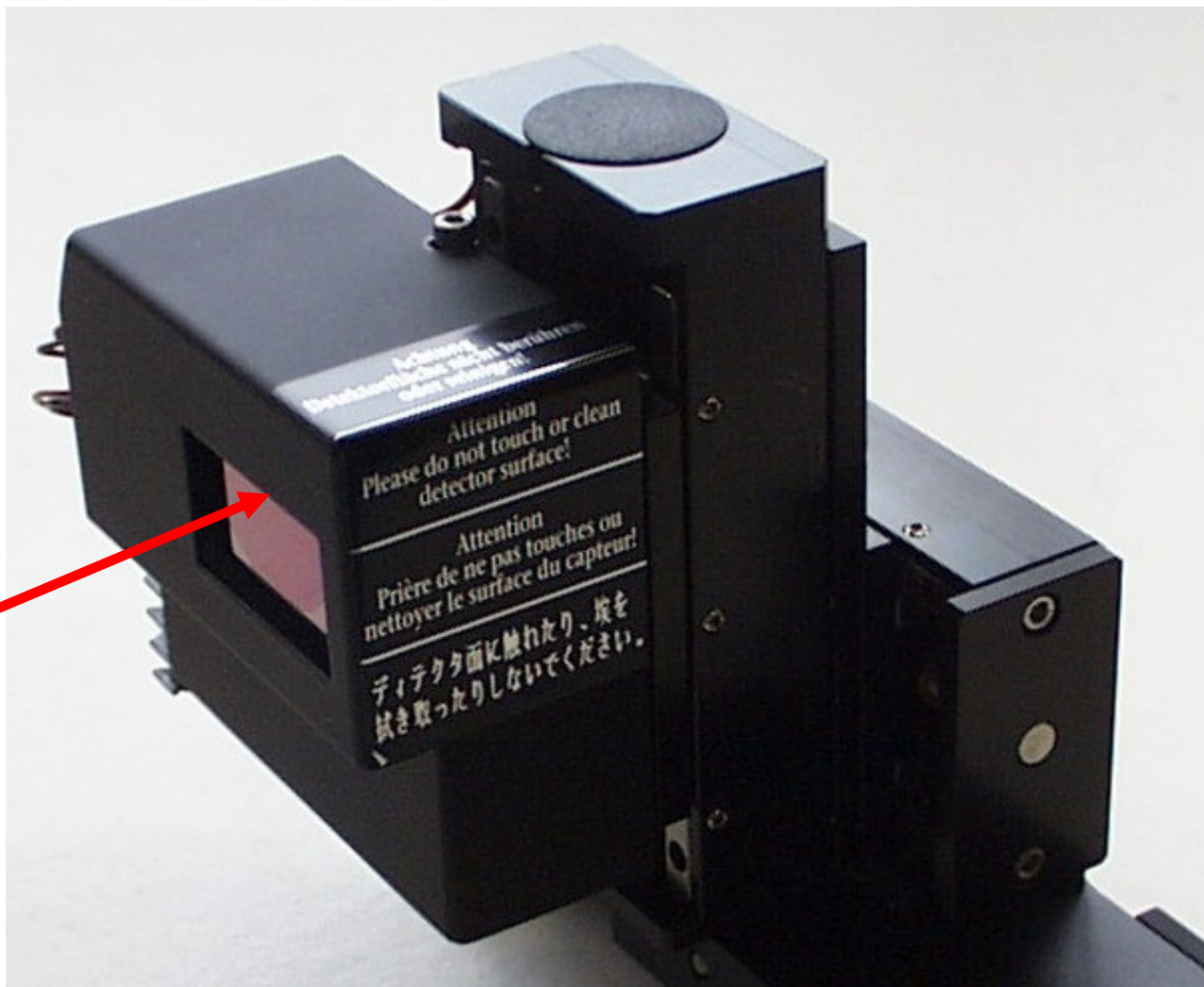
Multi-element detector with 31 classes and mono disperse intensity projection



**Design of
detector centre**



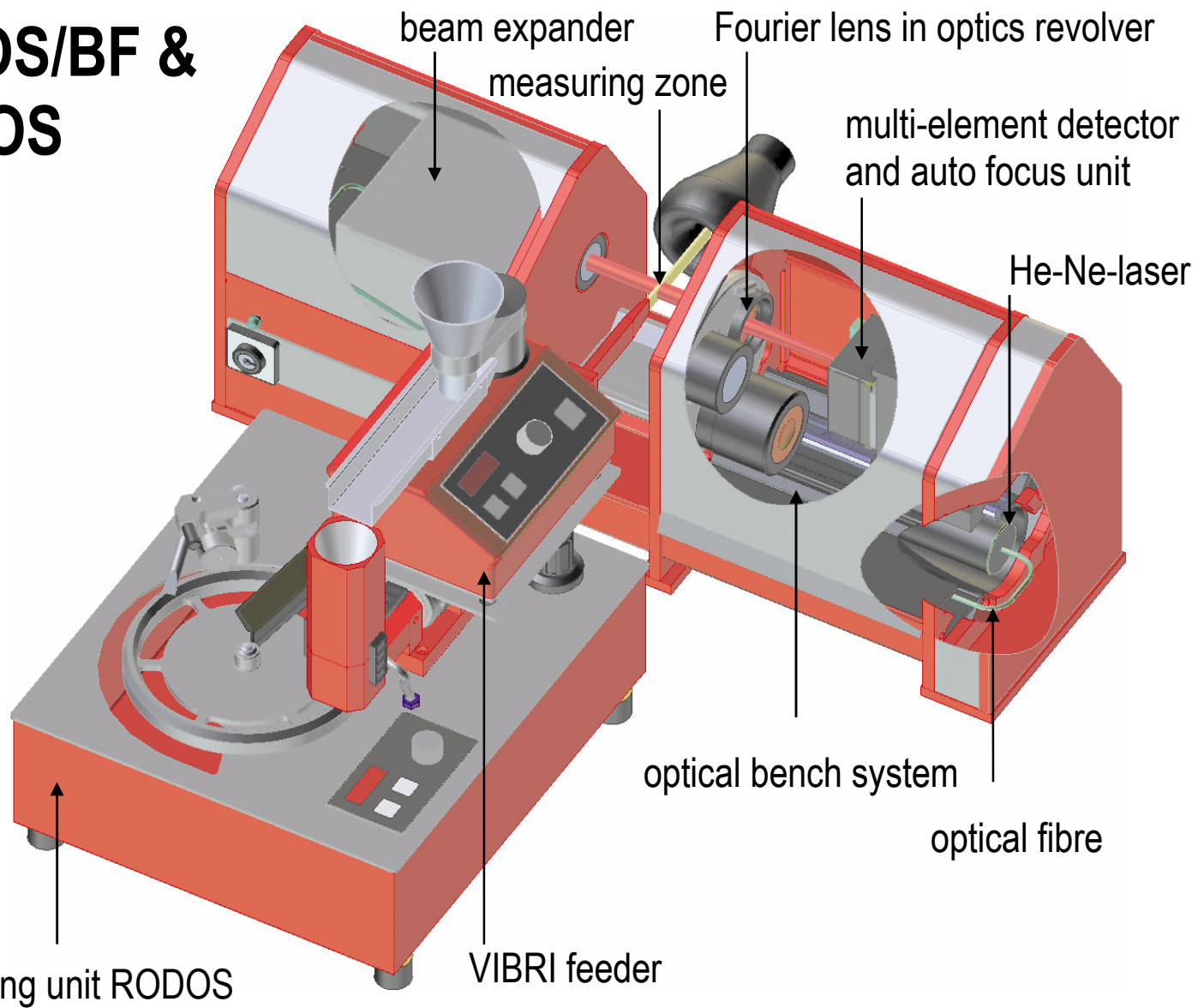
**Ideally centred
laser beam**



HELOS detector and auto-focus unit



HELOS/BF & RODOS



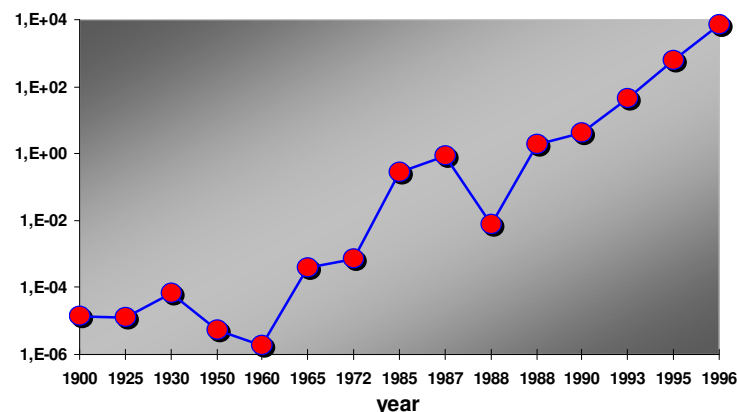
Comparison of Particle Size Analysis Methods

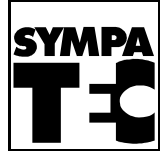
| year | method | dry | wet | x _{min} μm | x _{max} μm | Δx μm | Δx/x _{min} | t _A s | Δx/t _A μm/s | invest. T€ | Ω 1/(T€·μm·s) |
|------|-----------------------|-----|-------|------------------------|------------------------|----------|---------------------|---------------------|---------------------------|---------------|------------------|
| 1900 | sieving tower | x | | 100 | 10.000 | 9900 | 99 | 3600 | 2,75 | 5 | 1,38E-05 |
| 1925 | sedimentation balance | | x | 1 | 100 | 99 | 99 | 150.000 | 0,0007 | 13 | 1,32E-05 |
| 1930 | pipette | | x | 1 | 100 | 99 | 99 | 50.000 | 0,0020 | 8 | 6,60E-05 |
| 1950 | wet sieving | | x | 5 | 200 | 195 | 39 | 30.000 | 0,0065 | 13 | 5,20E-06 |
| 1960 | air jet sieve | x | | 30 | 1000 | 970 | 32 | 10.000 | 0,0970 | 15 | 1,80E-06 |
| 1965 | x-ray sedimentation | | x | 0,5 | 100 | 100 | 199 | 7200 | 0,0138 | 40 | 3,69E-04 |
| 1972 | laser diffraction | | x | 1 | 200 | 199 | 199 | 1500 | 0,1327 | 45 | 7,40E-04 |
| 1985 | laser diffraction | x | | 0,5 | 1750 | 1750 | 3499 | 100 | 17,50 | 65 | 2,80E-01 |
| 1987 | laser diffraction | | x | 0,1 | 100 | 100 | 999 | 60 | 1,67 | 50 | 8,40E-01 |
| 1988 | x-ray sedimentation | | x | 0,1 | 300 | 300 | 2999 | 2500 | 0,1200 | 40 | 7,50E-03 |
| 1988 | laser diffraction | | x | 0,1 | 700 | 700 | 6999 | 200 | 3,50 | 45 | 1,95E+00 |
| 1990 | laser diffraction | x | | 0,5 | 2625 | 2625 | 5249 | 10 | 262 | 65 | 4,04E+00 |
| 1993 | laser diffraction | x | | 0,25 | 3500 | 3500 | 13.999 | 5 | 700 | 60 | 4,48E+01 |
| 1995 | laser diffraction | x | | 0,1 | 8750 | 8750 | 87.499 | 5 | 1750 | 75 | 5,90E+02 |
| 1996 | laser diffraction | x | spray | 0,5 | 175 | 175 | 349 | 5E-04 | 349.000 | 50 | 7,00E+03 |

$$\Omega = \frac{\Delta x / x_{\min}}{x_{\min} \cdot t_A \cdot i} [(\text{€} \cdot \mu\text{m} \cdot \text{s})^{-1}]$$

- Δx : Measuring range (μm)
- x_{min} : Finest particle size
- t_A : Measuring time
- i : Cost for investment

Performance
Rate
Ω





Application of Laser Diffraction

| Stadium decade | Sensor & size ranges | Dispersing systems & product consciousness | Sampling & process coupling |
|-----------------------|---|--|--|
| Introduction 1970 | Basic application 1 - 200 μm | Suspension period | Exclusively via laboratory |
| Penetration 1980 | Sub-micron and extra millimetre 0.1–2000 μm | Fruitful dry period | Coupling with transport systems and samplers |
| Propagation 1990 | Completion of extension 0.1 – 8750 μm | Robotic era | Cultivation With sample couplers |
| Qualification 2000 | Standardisation ISO 13320 CFR21Part11 | Certification validation | Completion |



Fraunhofer Extension for Submicron Application

Examination of lower limit of Fraunhofer solution:

★ Established limit: $\alpha \gg 1$ (Mie factor $\alpha = \pi x/\lambda$)

what does it mean " \gg " ?
 is " $>$ " possible ?
 or even " \geq " ?

★ Study of the boundary condition: $\alpha = 1$

$\lambda = 632.8 \text{ nm} \Rightarrow x = 0.20 \text{ }\mu\text{m}$
 for liquids applies: $\lambda = \lambda_0/n$

★ Examples:

★ Advantages of Fraunhofer extension to $0.1 \text{ }\mu\text{m}$

- ☆ Independence of optical constants
 - * No need for determination
 - * No unknown relations
 - * No influence of changes on the result
- ☆ Only faint influence of shape on Fraunhofer solution
- ☆ Improved sensitivity due to less intensive matrix smoothing

| <i>Liquid</i> | Water | Tetrachlor ethylene |
|---|-------|---------------------|
| <i>Refractive index</i> | 1.330 | 1.504 |
| <i>Wave length [nm]</i> | 476 | 1.504 |
| <i>x ($\alpha = 1$) [μm]</i> | 0.151 | 0.134 |



The Theory of Mie

Conditions for Application of Mie's Theory to Particle Size Analysis

- ★ Knowledge of complex refractive index $m = n - ik$, comprising Refractive index (n) and absorption coefficient (ik)
- ★ Problems related to application of Mie's theory for particle size analysis:
 - ☆ Related to the particles:
 - * Applicable to spherical particles only
 - * Unknown refractive index and absorption coefficient
 - * Changes of the refractive index during the production process due to concentration and temperature
 - * Mixtures of particles with different m and unknown mixing ratio
 - * Influence of coated particles
 - ☆ Related to the mathematical algorithm:
 - * Unpredictable consequences on algorithm for non-spherical particles
 - * Highly different matrices due to smallest changes of m
 - * New matrix determination in any case
 - * Poor conditioning of matrices requests intensive smoothing procedure



HELOS MIE Software module

- ★ Complete realisation of exact Mie Theory
- ★ Matrices determined for continuous range of complex refractive indices m
= $n - ik$

- ☆ Available for all known materials

$$0.01 \leq n \leq 3.0$$

$$0.00 \leq k \leq 5.0$$

- ★ Evaluation time per set of parameters ≤ 1 second
- ★ Virtually no delay time
 - ☆ Study of parameter variations for extremely wide boundaries feasible
- ★ Easy selection of Mie parameters via HELOS software menu
- ★ Available for focal distances: $f = 20, 50, 100, 200$ mm
- ★ Available for laser wave lengths: $\lambda = 632.8, 670, 685$ nm
- ★ Requires not more than 5 Mbytes disk space per size range
- ★ Software tool:
 - ☆ Applicable to all HELOS sensor configurations
 - ☆ No hardware modifications necessary



HELOS MIE Software module

Check List:

- ✓ Refractive index n of particles and fluid known ?
 - ✓ Absorption coefficient k of particles known ?
 - ✓ No mixtures of different components ?
 - ✓ Spherical particles ?
 - ✓ Smooth particles surface ?
- ↪ Application of HELOS MIE Software for most precise results

However:

Due to rare availability of requested parameters, in practice very few cases of useful application only, e.g. beads, droplets

